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A BASIC PROPERTY OF MOS TRANSISTORS AND ITS CIRCUIT IMPLICATIONS

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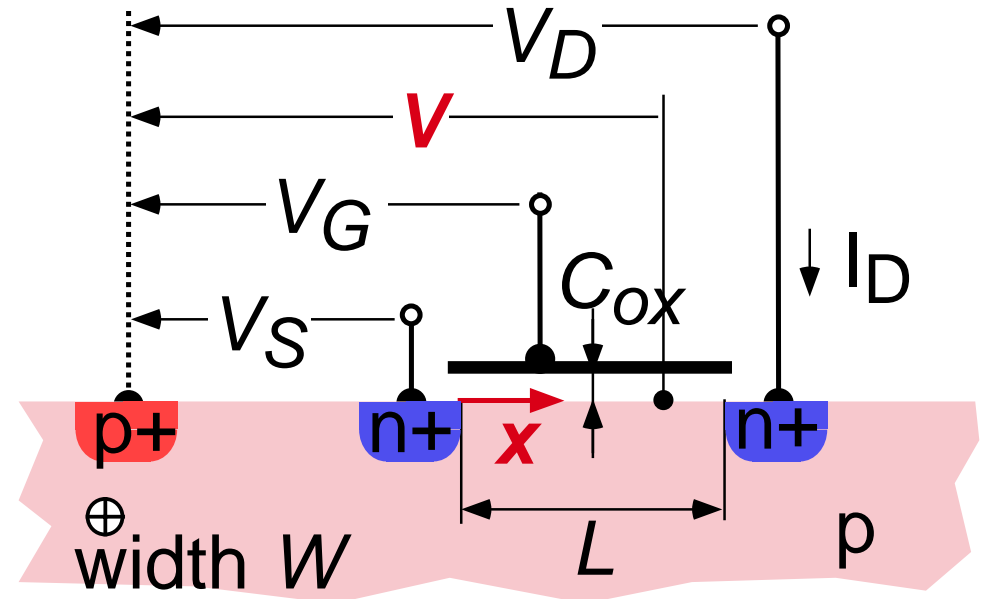
INTRODUCTION

- Goals of transistor modeling:
 - simulation by quantitative calculation on computer
 - highlighting properties to facilitate
 - understanding circuits
 - synthesis of robust circuits
- Best models: combine both goals by hierarchical structure
example: EKV model.
- EKV approach will be used to explicit a basic property.

DEFINITIONS

for EKV model

- Substrate referred-voltages
 V_S, V_D, V_G



- Local "channel voltage" V
splitting of quasi-Fermi levels due non-0 V_S and/or V_D

$$V = V_S \text{ at source}$$

$$V = V_D \text{ at drain}$$

n-channel: holes at equilibrium

thus $V = \text{electron quasi-Fermi level} + \text{constant}$.

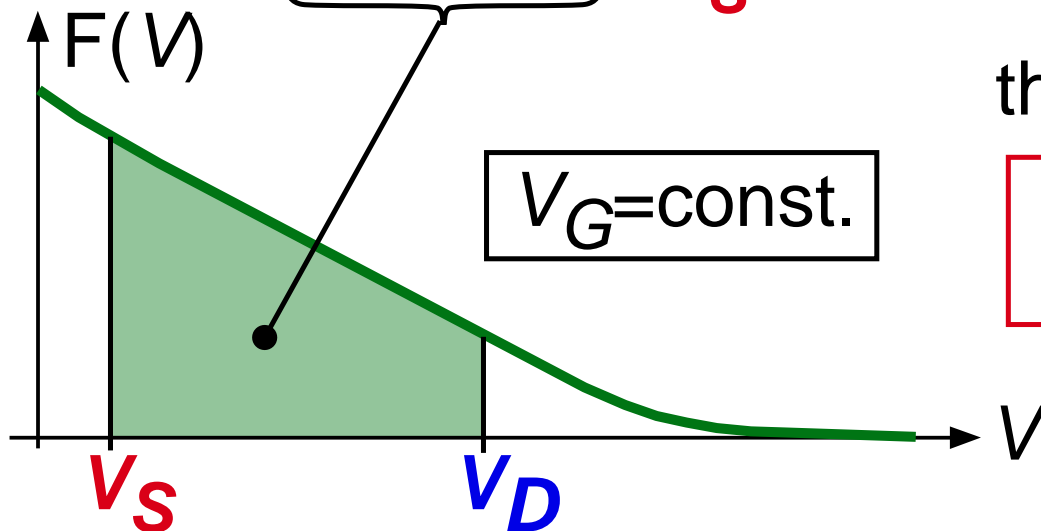
BASIC PROPERTY (1)

- For a long and wide channel:

$$I_D = \mu W(-Q_i) \frac{dV}{dx} \stackrel{=}{=} \frac{F(V, V_G)dV}{G(x, V_G)dx}$$

- Condition: **separable** in V and x

$$\text{then: } I_D \int_0^L G dx = \int_{V_S}^{V_D} F dV \equiv \int_{V_S}^{\infty} F dV - \int_{V_D}^{\infty} F dV$$



thus:

$$I_D = I(V_S, V_G) - I(V_D, V_G)$$

BASIC PROPERTY (2)

$$I_D = I(V_S, V_G) - I(V_D, V_G)$$

- The drain current is the **superposition** of **independent** and **symmetrical** effects of source and drain voltages.
- Definitions:
 - **Forward** current $I_F = I(V_S, V_G)$, independent of V_D
 - **Reverse** current $I_R = I(V_D, V_G)$, independent of V_S

$$\text{then } I_D = I_F - I_R$$

DOMAIN OF VALIDITY (2)

- Condition:

$$\mu W(-Q_j) = \frac{F(V, V_G)}{G(x, V_G)}$$

- W is independent of V ; thus:
 - part of G , may depend on x : \Rightarrow any shape of channel.
- Mobility μ depends on vertical field thus on Ψ_S , thus
 - included in F , provided velocity $v \ll v_{sat}$
(otherwise depends on I_D itself)
- Furthermore, the effective value of L along which $G(x, V_G)$ is integrated must be independent of I_D , V_S and V_D .

EFFECT OF NARROW CHANNEL

- Increased importance of side effects.
- Equivalent to parallel connection of several transistors with different characteristics.
 - if each transistor i fulfils

$$I_{Di} = I_i(V_S, V_G) - I_i(V_D, V_G)$$

- then the sum I_D of I_{Di} fulfils it as well.
- The property is not degraded.

DOMAIN OF VALIDITY (SUMMARY)

The basic property is available

- For **long** and **homogeneous** channel
- Independently of channel shape
- Even if the channel is very narrow
- Even for large gate voltages reducing the mobility.

CAUSES OF DEGRADATION (1)

- Non homogeneous channel: Q_i direct function of x .

$$Q_i = -C_{ox}(V_G - V_{FB} - \Psi_s) + \sqrt{2q N_b \epsilon_{si} \Psi_s}$$

There may be variations with position x in the channel of:

- substrate doping N_b , which can be
 - intentional (e.g.: LDD)
 - artifact of process (gradient or piling-up)
(always present at very ends of channel)
- flat-band voltage V_{FB} , caused by
 - variation of N_b
 - variation of charge in oxide
- effective C_{ox} , always present at very ends of channel.

SPECIAL CASE OF WEAK INVERSION

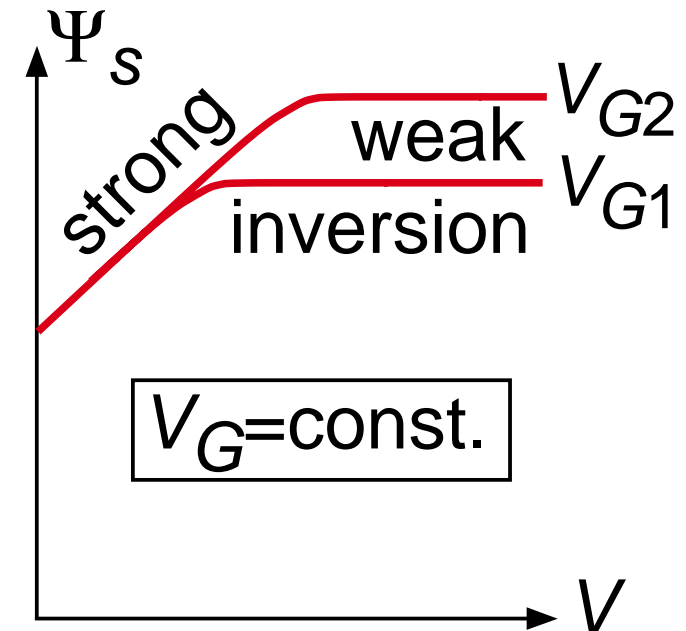
- Weak inversion characterized by $Q_i \ll Q_b$, therefore:
 - Q_i has negligible effect on potential and field

- Can be expressed as $-Q_i = G_q(\Psi_s)e^{-V/U_T}$

- with Ψ_s independent of V , thus:

- G_q can be any function of x and is included in G , therefore:

- The property is valid even if the channel is not homogeneous.



- Mobility μ independent of V , thus part of G ,
 F is reduced to $F = e^{-V/U_T}$: independent of V_G .

CAUSES OF DEGRADATION (2)

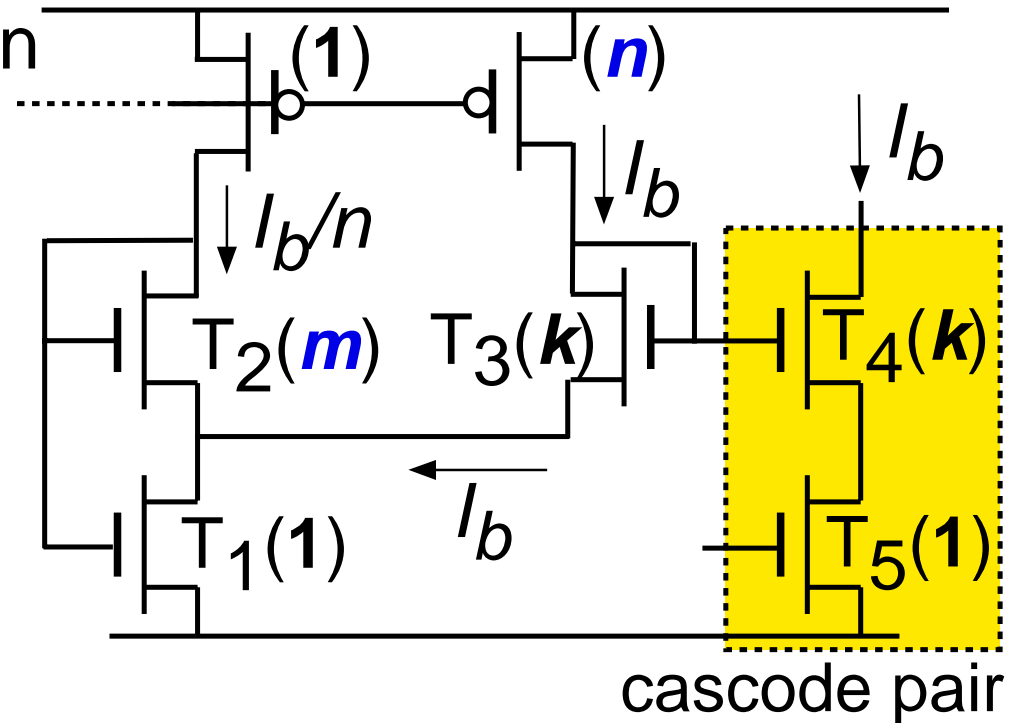
- Channel long \Rightarrow non-long \Rightarrow short
 - property progressively degraded by...
 - several independent mechanisms:
 - a.** Voltage effects:
 - channel length modulation
 - I_F or I_R becomes function of both V_D and V_S
 - effect proportional to $1/L$
 - barrier lowering and 2-D effects: further degradation.
 - b.** Current effects:
 - if I_D is increased by reducing L , then
 - \Rightarrow carrier velocity increases towards saturation
 - \Rightarrow mobility reduced, thus function of I_D
 - c.** Non-homogeneous channel (except in weak inversion):
 - importance of end-effects proportional to $1/L$.

CIRCUIT EXAMPLE: LOW-VOLTAGE CASCODE

- Goal: V_{D5} min. for saturation

- Means: control $\frac{I_{R5}}{I_{F5}} \ll 1$:

- m and $n \gg 1$, hence:
- $I_{D5} \cong I_{D1}$ with $V_{D5} = V_{D1}$
- thus $I_{R5}/I_{F5} \cong I_{R1}/I_{F1}$



$$\left. \begin{array}{l} \bullet I_{F2} = I_b/n = m I_{R1} \\ \bullet I_{F1} \cong I_b \end{array} \right\} \Rightarrow \frac{I_{F1}}{I_{R1}} \cong \boxed{mn} \cong \frac{I_{F5}}{I_{R5}}$$

- Large enough to ensure saturation
- Independent of I_b .

CONCEPT OF PSEUDO-RESISTOR

- We have shown that:
$$I_D = \frac{1}{\int_0^L G dx} \left[\int_{V_S}^{\infty} F dV - \int_{V_D}^{\infty} F dV \right]$$

- Definitions:
 - pseudo-voltage:
$$V^* = -K_0 \int_V^{\infty} F(V, V_G) dV$$

- pseudo-resistor:
$$R^* = K_0 \int_0^L G(x, V_G) dx$$

(where K_0 : any positive constant)

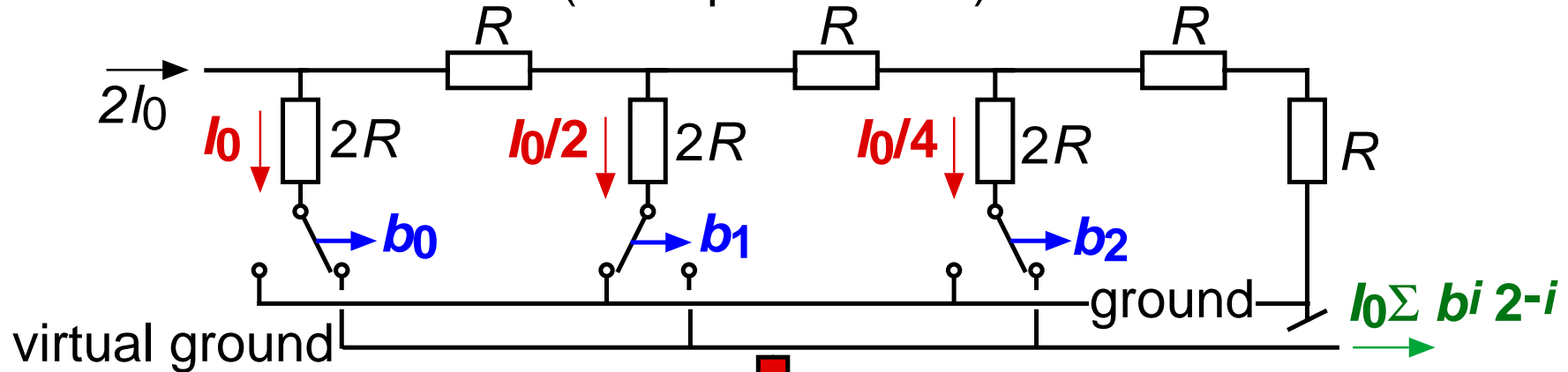
- Results in pseudo Ohm's Law:
$$I_D = (V_D^* - V_S^*)/R^*$$

LINEAR CURRENT-MODE CIRCUITS

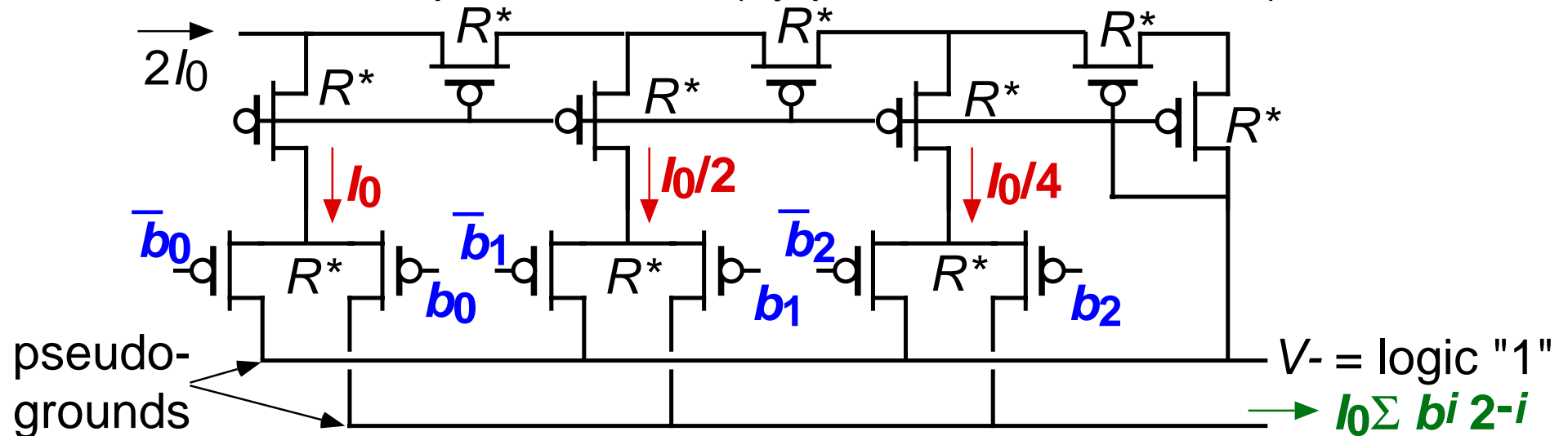
- Implications of pseudo Ohm's law $I_D = (V_D^* - V_S^*)/R^*$
 - Any network interconnecting transistors with same $F(V, V_G)$ and **same V_G** is **linear with respect to currents**.
 - Any circuit of linear resistors can be implemented by **transistors only**, provided only currents are considered.
 - A resistor connected to ground ($V=0$) in the resistive prototype corresponds to a **saturated** transistor that provides a **pseudo-ground** ($V^*=0$).
- In weak inversion:
 - F indep. of V_G , but V_G included in function G , hence:
 - **Different V_G possible** for each transistor
 - Each **R^* can be separately adjusted** by its V_G .

EXAMPLE OF APPLICATION: R-2R D/A CONVERTER

- Standard resistive circuit (example for 3-bit): [6,7]



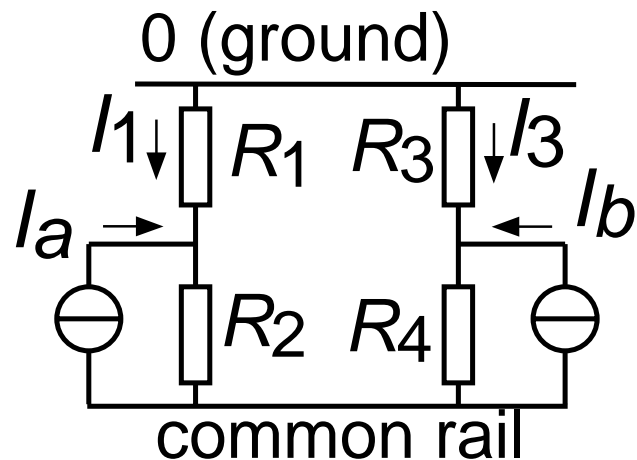
- Pseudo-resistive implementation (by p-channel transistors):



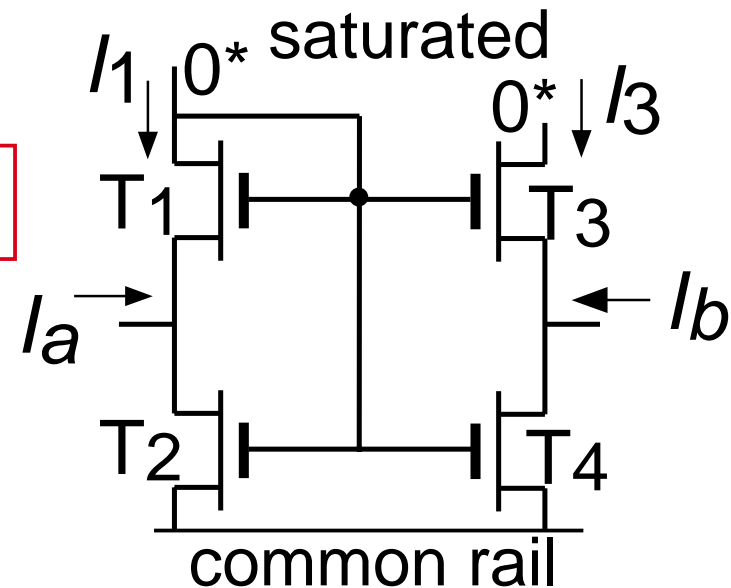
- For best precision:
 - strong inversion
 - non-saturated devices (avoid pseudo-grounds)

APPLICATION OF PSEUDO-RESISTORS

(example)



$$R_i \sim L_i / W_i$$



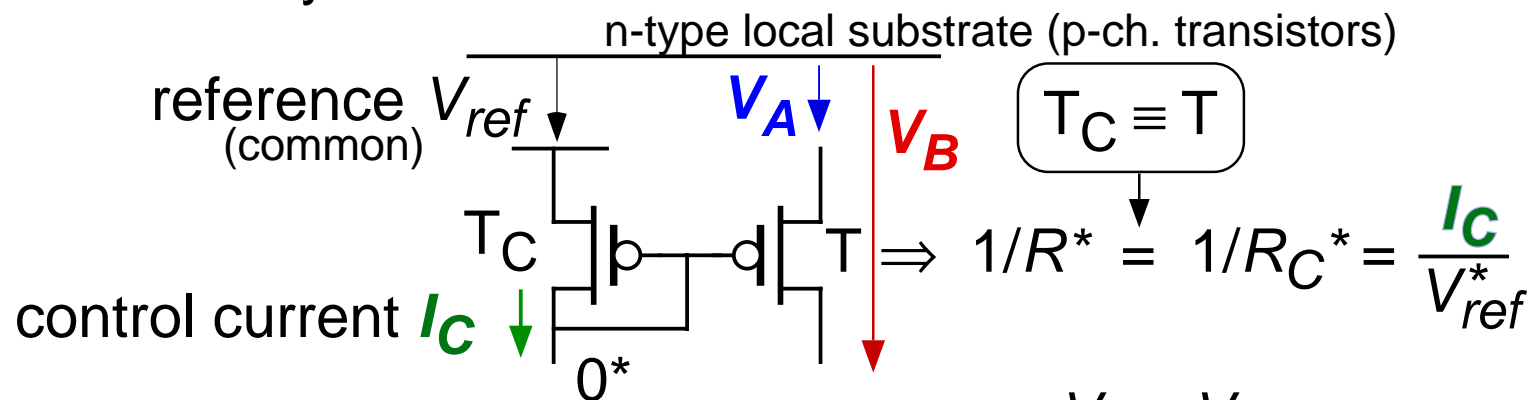
$$(R_3 + R_4)I_3 + R_4I_b = (R_1 + R_2)I_1 + R_2I_a$$

thus:
$$I_3 = k_1 I_1 + k_a I_a - k_b I_b$$

- Output I_3 is the **weighted sum** of I_1 , I_a and $-I_b$.
- I_a is **low-voltage** input (T_2 not saturated)
- For $R_4=0$ (T_4 in s/c) and $T_1=T_2=T_3 \Rightarrow k_1 = 2$
 - for N unit trans. in series at input $\Rightarrow k_1 = N$
 - for M units in parallel at output $\Rightarrow k_1 = **M.N**$

PSEUDO-RESISTORS IN WEAK INVERSION

- If I_F and $I_R \ll I_S = 2n\beta U_T^2 \rightarrow$ weak inversion
- Then: $I(V_G, V) = I_S \exp \frac{V_G - V_{T0}}{nU_T} \exp \frac{-V}{U_T}$ **separable** in V_G and V
- Therefore:
 - pseudo-voltage $V^* = -V_0 \exp \frac{-V}{U_T}$ **independent** of V_G
 - pseudo-conductance $1/R^* = \frac{I_S}{V_0} \exp \frac{V_G - V_{T0}}{nU_T}$ **controllable** by V_G
- Low voltage swing (in wide current range), thus compatible with **low V_B**
- Control of R^* by a current:

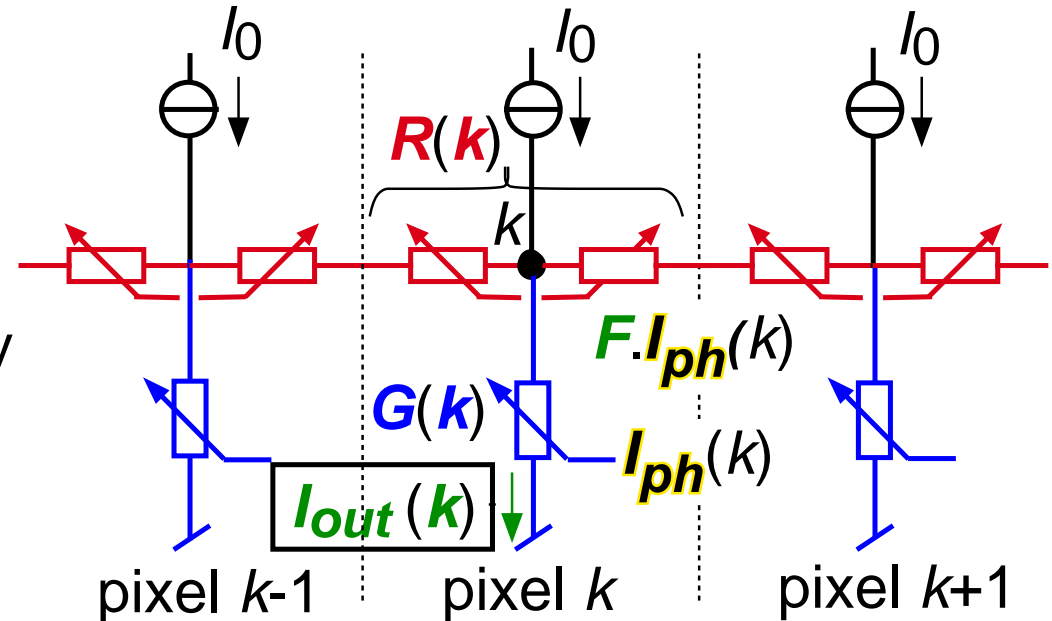


- weak inversion ensured if $I_C \exp \frac{V_{ref} - V_{A(B)}}{U_T} \ll I_S$

EXAMPLE OF APPLICATION: LOCALLY ADAPTIVE RETINA

[97-1]

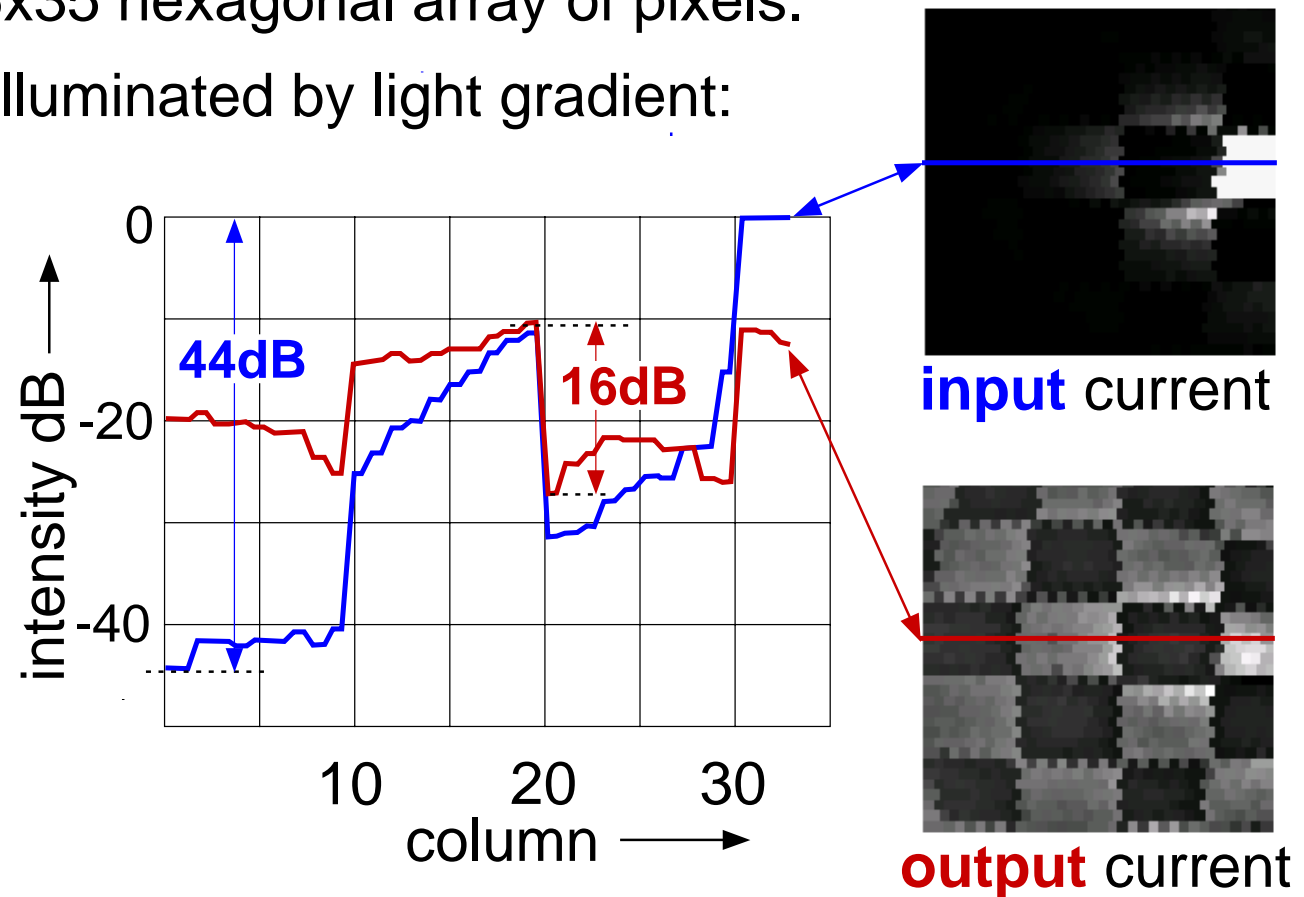
- Schematic for 1-D array:
- Real implementation: 2-D array with $R, G \rightarrow R^*, G^*$ (pseudo-resistors)



- $G(k)$ proportional to $I_{ph}(k)$ (local photocurrent)
 - $1/R(k)$ proportional to $F \cdot I_{ph}(k)$
- If $R(k) = 0$ then $\sum I_{out}(k) = \sum I_0$: global normalisation
- If $R(k) > 0$, each I_0 distributed across area $A \sim L^2 = 1/(RG) \sim F$
 - **local normalisation** in adjustable area A .

MEASUREMENTS ON LOCALLY ADAPTIVE RETINA

- Experimental 35x35 hexagonal array of pixels.
- Checker-board illuminated by light gradient:

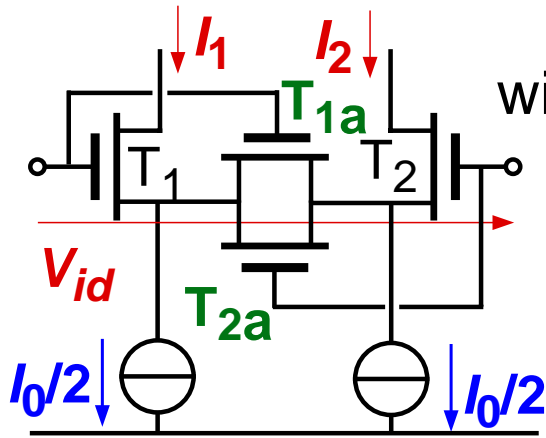


- Dynamic range reduced to that of the object **contrast** (independently of light distribution).

LINEARIZATION OF DIFFERENTIAL PAIR BY TRANSISTORS

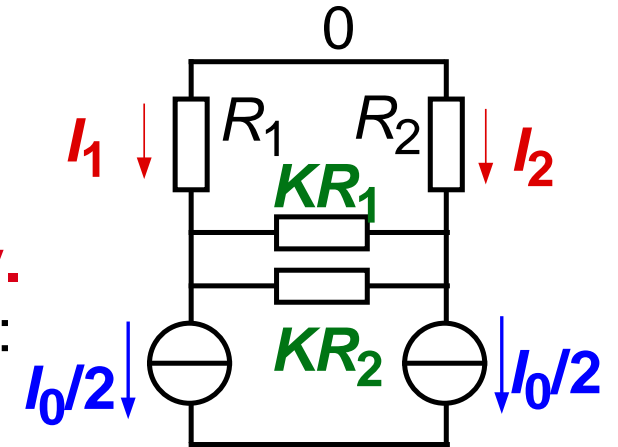
LVT-18

[13]



with $\frac{\beta_1}{\beta_{1a}} = \frac{\beta_2}{\beta_{2a}} = K$

Equivalent circuit in **weak inv.**
(concept of pseudo-resistors):

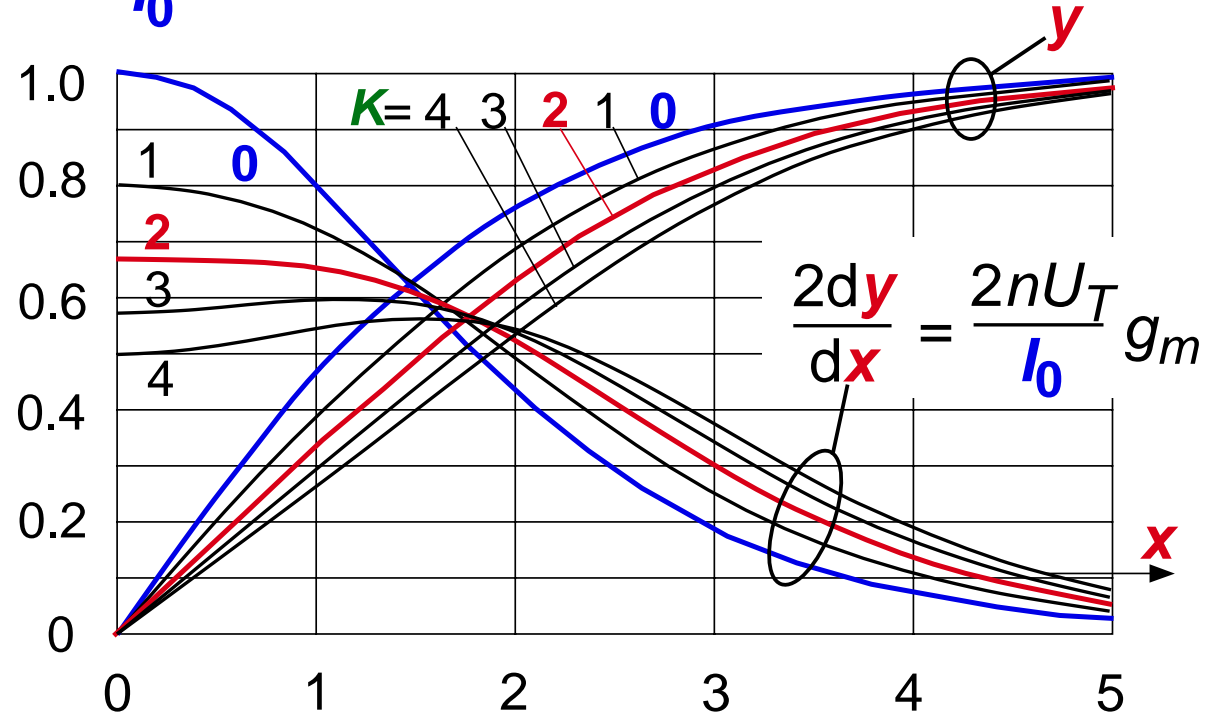


definitions: $x = \frac{V_{id}}{nU_T}$ and $y = \frac{I_1 - I_2}{I_0}$ then: $R_2/R_1 = e^x$

• Results in:

$$y = \frac{e^x - 1}{e^x + 1 + K \frac{e^x}{e^x + 1}}$$

• Also applicable in strong inversion



FURTHER APPLICATIONS OF PSEUDO-RESISTORS

- Linear attenuators (electrical control in weak inversion)
 - R-2R network for D/A conversion.
- Spatial information processing:
 - n^{th} order moment computation
 - diffusion networks (isotropic or not)
 - 2-D emulation of physical media
 - path finding.
- In weak inversion: exploitation of current distribution in voltage- (or current-) dependent linear networks:
 - local normalisation in vision processing
 - generation of nonlinear functions
 - ...

CONCLUSION

- Basic MOS property for long and homogeneous channels:

$$I_D = I(V_S, V_G) - I(V_D, V_G) = I_F - I_R$$

- superposition of independent and symmetrical effects of S and D voltages.
- forward and reverse components.
- Property progressively degraded when channel shortened.
- Underlies the concept of pseudoresistor:
 - linear current mode circuits
 - transistor implementation of arrays of resistors.
 - simpler analysis of transistor circuits.

POST-SCRIPTUM: INGREDIENTS OF DC CORE OF EKV MODEL

- Voltages referred to (local) substrate
- Quasi-Fermi level of channel carriers V
- Gradual channel and charge sheet approximations
- Mobile ch. density $Q_i = -C_{ox}[V_G - V_{TB}(\psi_s)]$
- $\psi_s = \psi_0 + V$ in strong inversion (independent of V_G)
- Pinch-off value of V : $V_P(V_G) = \psi_P(V_G) - \psi_0$
- Linearization of $Q_i(\psi_s) \Rightarrow n \cong \text{constant}$
- General expression of $Q_i(V_P - V)$
- $I_D \approx \int_{V_S}^{V_D} Q_i dV = I(V_G, V_S) - I(V_G, V_D) = I_F - I_R$
- Specific current $I_S = 2n\beta U_T^2$
- Inversion coeff. $IC = \text{the larger of } I_F/I_S \text{ or } I_R/I_S$

