

EE140 HW#8 Solution

①

1.

a) At the operation frequency ω_0 of 106 rad/s

L_g , C_{gs} & L_s is resonant. The gate to source voltage is Q times as large as the input voltage. So the overall stage transconductance G_m under this condition is:

$$\begin{aligned} G_m &= Q \cdot g_{m1} = \frac{1}{R_s + \frac{g_m(L_g + L_s)}{C_{gs}}} \cdot g_{m1} \\ &= \frac{1}{100 \Omega} \times 23.45 \text{ mS} \\ &= 3.5 \text{ mS} \end{aligned}$$

$$\therefore A_{vo} = G_m \cdot Z_{out}$$

At ω_0 , L_p & C_L in resonant $\therefore Z_{out} = R_{out} = 100 \Omega$

$$\therefore A_{vo} = G_m \cdot R_{out} = 3.5$$

$$b) \quad Z_{in} = sL_s + \frac{1}{sC_{gs}} + \frac{g_m}{C_{gs}} \cdot L_s + s \cdot L_g \quad (2)$$

Substitute $s = 10^6 \text{ rad/s}$ $g_m = 23.45 \text{ mS}$
 $C_{gs} = 0.67 \text{ pF}$

$$Z_{in} = 50 \Omega$$

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2.

For M_1 & M_6 :

$$I_D = \frac{1}{2} \mu C_{ox} \frac{W}{L} (V_{GS} - V_t)^2$$

$$100 \mu\text{A} = 15 \mu\text{A} \times 50 \times (V_{GS} - V_t)^2$$

$$\therefore V_{GS} = -1.065 \text{ V}$$

For M_3 , M_5 & M_7 .

$$100 \mu\text{A} = 30 \mu\text{A} \times 50 \times (V_{GS} - V_t)^2$$

$$V_{GS} = 0.958 \text{ V}$$

$$\therefore V_{SG2} = 5 \text{ V} - 1.065 \text{ V} - 0.958 \text{ V} = 2.977 \text{ V}$$

$$\therefore 100 \mu\text{A} = 15 \mu\text{A} \cdot \left(\frac{W}{L}\right)_2 (2.977 - 0.7)^2$$

$$\therefore \left(\frac{W}{L}\right)_2 = 1.286 = \frac{2.57 \mu\text{A}}{2 \mu\text{A}}$$

$$2.5 \text{ V} = V_{GS4} + V_{GS7}$$

$$\therefore 2.5 \text{ V} - 0.958 \text{ V} = 1.542 \text{ V} = V_{GS4}$$

$$V_{t4} = V_{t0} + \gamma (\sqrt{2\phi_f + V_{SB}} - \sqrt{2\phi_f})$$

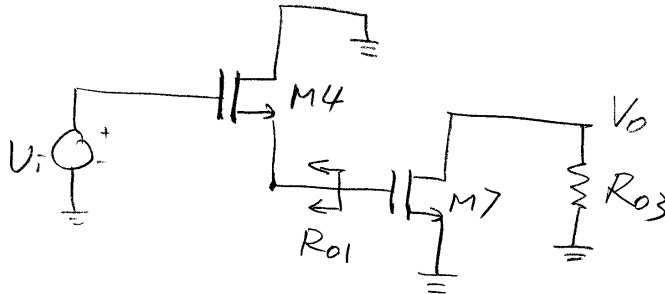
$$= 0.7 \text{ V} + 0.4 \times (\sqrt{0.6 + 0.958} - \sqrt{0.6})$$

$$= 0.89 \text{ V}$$

$$I_{D4} = 100\mu\text{A} = 30\mu\text{A} \times \left(\frac{W}{L}\right)_4 (1.542 - 0.89)^2 \quad (4)$$

$$\therefore \left(\frac{W}{L}\right)_4 = 7.83 = \frac{15.7\mu}{2\mu}$$

Signal path:



$$R_{o1} = \frac{1}{g_{m4} + g_{mb4}}$$

$$g_{m4} = \sqrt{2I_{D4}\mu C_{ox}\frac{W}{L}} = \sqrt{200\mu\text{A} \times 60\mu\text{A/V}^2 \times 7.83} = 307\mu\text{A/V}$$

$$g_{mb4} = g_{m1} \cdot \frac{\gamma}{2\sqrt{2\phi_f + V_{SB}}} = 307\mu\text{A/V} \times \frac{0.4}{2\sqrt{0.6 + 0.958}} = 49.2\mu\text{A/V}$$

$$\therefore R_{o1} = 2811\Omega$$

$$g_{m7} = \sqrt{200\mu\text{A} \times 60\mu\text{A/V}^2 \times 50} = 775\mu\text{A/V}$$

$$R_{o3} = r_{o7} \parallel r_{o6} = \frac{1}{0.03 \times (100\mu\text{A})} \parallel \frac{1}{0.03 \times (100\mu\text{A})} = 167\text{k}\Omega$$

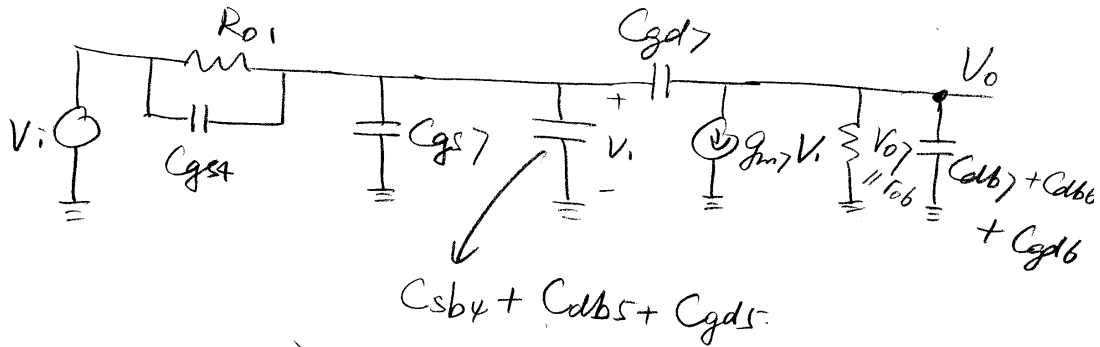
$$\therefore \text{gain} = \frac{V_o}{V_i} = \frac{g_{m4} R_s}{1 + g_{m6} R_s} \cdot -g_{m7} \cdot R_{o3}$$

$$R_s = r_{o7} = 333 \text{ K}$$

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$$\therefore \frac{V_o}{V_i} = - \frac{307 \mu \times 333 \text{ K}}{1 + 307 \mu \times 333 \text{ K}} \times 725 \mu \times 167 \text{ K}$$

$$= -128.1$$



$$C_{sb4} = \frac{C_{sb0}}{\sqrt{1 + \frac{V_{sB}}{4_0}}} = \frac{0.8 \text{ f} (7.83)}{\sqrt{1 + \frac{0.958}{0.6}}} = 3.89 \text{ fF}$$

$$C_{db5} = \frac{0.8 \text{ f} (100)}{\sqrt{1 + \frac{0.958}{0.6}}} = 49.6 \text{ fF}$$

$$C_{gd5} = 0.3 \times 100 \text{ f} = 30 \text{ fF} = C_{gd7}$$

$$C_{gs7} = \frac{2}{3} WL C_{ox} + 30 \text{ fF} = 261 \text{ fF}$$

$$C_{db7} = \frac{C_{db0}}{\sqrt{1 + \frac{V_{sB}}{4_0}}} = 35.2 \text{ fF} = C_{db6}$$

$$R_{o1} (C_{sb4} + C_{db5} + C_{gd5} + C_{gs7}) = 0.968 \text{ nS}$$

$$(r_{o7} \parallel r_{o6}) (C_{db7} + C_{db6} + C_{gd6}) = 16.8 \text{ nS}$$

$$C_{gd7} (R_{o1} + R_{o3} + g_{m2} R_{o1} R_{o3}) = 16 \text{ nS} \quad (6)$$

$$\therefore f_{-3\text{dB}} = \frac{1}{2\pi} \cdot \frac{10^9}{0.968 + 16.8 + 16} = \underline{\underline{4.71 \text{ MHz}}}$$

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3. For the circuit a. there are two poles associated with input and output node.

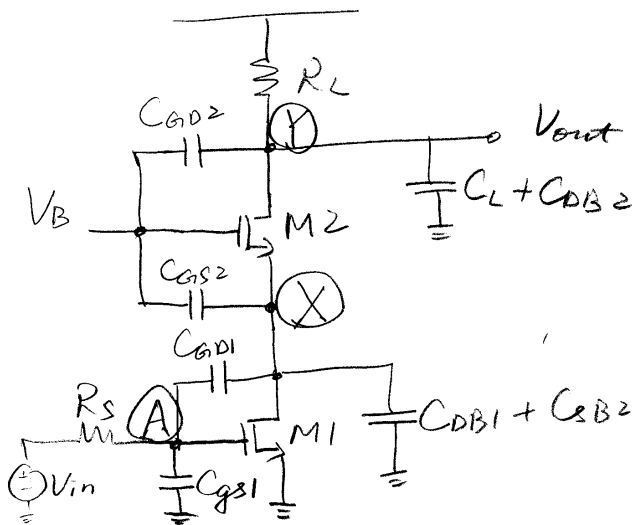
At input, since $R_L C_L \ll g_{m1} R_L R_S C_{gd}$, do the miller approximation

$$P_{input} = \frac{1}{g_{m1} R_L R_S C_{gd} + R_S C_{gs}} \leftarrow \text{dominant pole}$$

At output.

$$P_{output} = \frac{1}{R_L C_L} \leftarrow \text{second pole}$$

For the circuit b. we can draw the equiv. model shown below.



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The pole associated with node A is estimated as:

$$\omega_{p,A} = \frac{1}{R_s \left[C_{GS1} + \underbrace{\left(1 + \frac{g_{m1}}{g_{m2} + g_{mb2}} C_{GD1} \right)}_{\text{Miller approximation}} \right]} \quad \leftarrow \begin{array}{l} \text{dominant} \\ \text{pole} \end{array}$$

the pole associated with node X is:

$$\omega_{p,X} = \frac{g_{m2} + g_{mb2}}{2C_{GD1} + C_{DB1} + C_{SB2} + C_{GS2}}$$

Finally, there is a pole associated with output

$$\omega_{p,y} = \frac{1}{R_L (C_{DB2} + C_L + C_{GD2})}$$

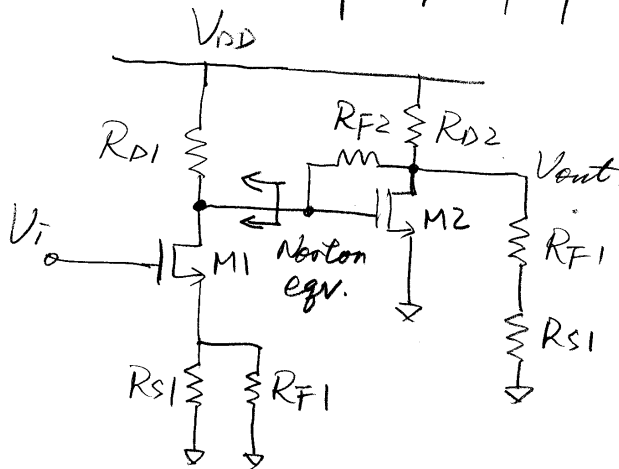
Compare the dominant pole of two circuits.

We find out that by cascoding, circuit frequency response has been greatly improved.

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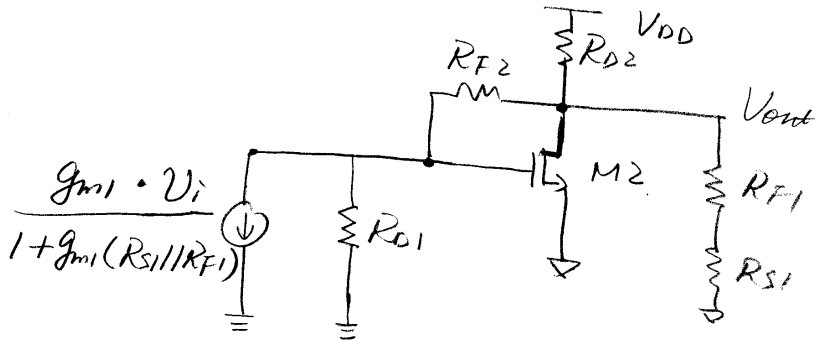
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- a) There are two feedback loops in this circuit. The external feedback include $M1, M2, R_{F1}$ & R_{S1} . Internal feedback is $M2$ & R_F .
- b) External feedback is series - shunt.
Internal feedback is shunt - shunt.
- c) For the external feedback loop, open the feedback loop w/ proper loading.

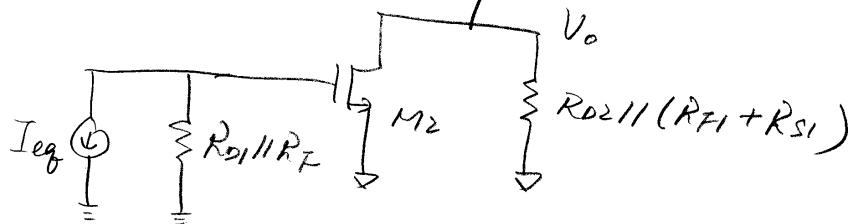


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Using Norton eqv. circuit to simplify the circuit. we have:



Open the internal loop:



$$\therefore \left(\frac{V_o}{I_{eq}} \right)_{OL} = g_{m2} \cdot (R_{D2} \parallel (R_{F1} + R_{S1})) \cdot (R_{D1} \parallel R_F)$$

$$f = \frac{1}{R_{F2}}$$

$$\therefore \left(\frac{V_o}{I_{eq}} \right)_{CL} = \frac{\left(\frac{V_o}{I_{eq}} \right)_{OL}}{1 + f \cdot \left(\frac{V_o}{I_{eq}} \right)_{OL}} = \frac{g_{m2} \cdot (R_{D2} \parallel (R_{F1} + R_{S1})) \cdot R_{D1}}{1 + \frac{1}{R_{F2}} \cdot g_{m2} \cdot (R_{D2} \parallel (R_{F1} + R_{S1})) \cdot (R_{D1} \parallel R_F)}$$

$$\left(\frac{V_o}{I_{eq}}\right)_{CL} = \frac{V_o}{\frac{g_{m1} \cdot V_i}{1 + g_{m1}(R_{S1} \parallel R_{F1})}}$$

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$$\therefore \left(\frac{V_o}{V_i}\right)_{OL} = A = \frac{g_{m1}}{1 + g_{m1}(R_{S1} \parallel R_{F1})} \cdot \left(\frac{V_o}{I_{eq}}\right)_{CL}$$

$$= \frac{1}{200} \times \frac{1}{1 + \frac{1}{200} \times 1K\Omega} \times \frac{1}{200} \times (1K \parallel 2K) \times 0.5K$$

$$= \frac{1}{1.2K} \times \frac{\frac{5}{3}K}{1 + \frac{5}{6}} = \underline{\underline{757.6}}$$

$$f = \frac{R_{S1}}{R_{S1} + R_{F1}} = \underline{\underline{\frac{1}{2}}}$$

$$T = A \cdot f = \underline{\underline{378.8}}$$

$$d) \left(\frac{V_o}{V_i}\right)_{CL} = \frac{A}{1 + A \cdot f} = \frac{757.6}{388.8} = 1.949$$

$$R_{in} = \infty$$

$$R_{out} = \frac{R_{out}(OL)}{1 + T_{external}} = \frac{R_{F2} \parallel R_{D2} \parallel (R_{F1} + R_{S1})}{1 + T_{external}}$$

$$= \frac{1K\Omega \parallel 1K\Omega \parallel 2K\Omega}{(1 + 378.8) \left(1 + \frac{1}{2K} \times \frac{1}{200} \times (1K \parallel 2K) \times 0.5K\right)}$$

$$= \frac{0.41 \text{ k}\Omega}{\frac{11}{6} \times 388.8} = 0.56 \text{ }\Omega$$