

$$V_{O1} = V_{IC} + \frac{V_{ID}}{2}$$

$$V_{O2} = V_{IC} - \frac{V_{ID}}{2}$$

$$V_{O1} = V_{OC} + \frac{V_{OD}}{2}$$

$$V_{O2} = V_{OC} - \frac{V_{OD}}{2}$$

a).

$\because R_{SS} \gg R_2$ ,  $\frac{1}{g_m}$  of  $M_1, M_2$ ,  $\therefore$  all  $I_{SS}$  flows into diff. pair.

$$V_Y = V_X = V_{IC} - V_{t0} - V_{dsat} = V_{IC} - V_{t0} - \sqrt{\frac{I_{SS}/2}{\frac{1}{2}k' \frac{W}{L}}}$$

$$= V_{IC} - V_{t0} - \sqrt{\frac{I_{SS}}{k' \frac{W}{L}}} \quad *$$

$$V_X = V_Y - \frac{I_{SS}}{2} R_2 = V_{IC} - V_{t0} - \sqrt{\frac{I_{SS}}{k' \frac{W}{L}}} - \frac{I_{SS}}{2} R_2 \quad *$$

$$V_{O1} = V_{O2} = V_{DD} - \frac{I_{SS}}{2} R_1 \quad *$$

b)  $V_{ds1,2} \gg V_{dsat}$ .

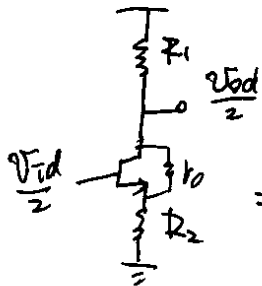
$$\therefore V_{DD} - \frac{I_{SS}}{2} R_1 - (V_{IC} - V_{dsat}) > V_{dsat}$$

$$\Rightarrow V_{IC} \leq V_{DD} - \frac{I_{SS}}{2} R_1 + V_{t0} \quad *$$

c) Calculate differential gain  $A_{cm} = \frac{V_{od}}{V_{id}}$ .

(2)

Half ckt. model. X is virtual ground.



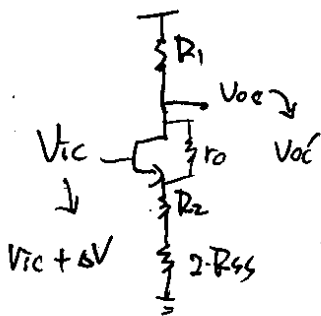
$$\frac{V_{od}}{2} = \frac{V_{id}}{2} \cdot \left( \frac{-g_m}{1 + g_m R_2} [r_o(1 + g_m R_2) \parallel R_1] \right)$$

$\Rightarrow$  CS with source degeneration.

$$\therefore \frac{V_{od}}{V_{id}} = - \frac{\sqrt{\mu} K' \frac{W}{L} I_{SS}}{1 + \sqrt{\mu} K' \frac{W}{L} I_{SS} R_2} \left( r_o (1 + \sqrt{\mu} K' \frac{W}{L} I_{SS} R_2) \parallel R_1 \right)$$

d) Common-mode gain  $A_{cm} = \frac{V_{oc}}{V_{ic}}$ .

Half ckt. model, similar to c), except source degeneration more



$$\frac{V_{oc}}{V_{id}} = - \frac{\sqrt{\mu} K' \frac{W}{L} I_{SS}}{1 + \sqrt{\mu} K' \frac{W}{L} I_{SS} (R_2 + 2R_{SS})} \left( r_o (1 + \sqrt{\mu} K' \frac{W}{L} I_{SS} (R_2 + 2R_{SS})) \parallel R_1 \right)$$

$$= A_{cm} \quad \times$$

change in  $V_{ic}$  will cause the same voltage drop at outputs, therefore, only output common mode ( $V_{oc}$ ) change, not the differential mode ( $V_{od}$ )!

$$\therefore V_{oc} = V_{oc} + A_{cm} \cdot \Delta V = \frac{V_{o1} + V_{o2}}{2} - A_{cm} \cdot \Delta V$$

$\times$